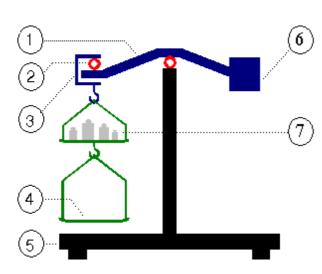
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# Basic scale and balance technology

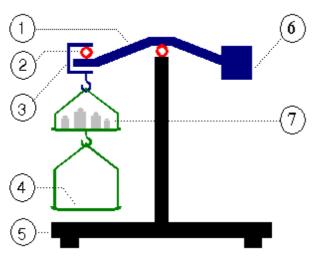
The most simple and well known weighing instrument is the classical analytical balance below:



- 1 = arm
- 2 = hinged joint (suspension point)
- 3 = pan carrier
- 4 = suspended weighing pan
- 5 = housing

By placing an object on one pan it can be compared with a weight placed on the other pan. When the object or the weight is not placed in the center of the pan, the pan will move so that the center of gravity is below the suspension point. So there is no error caused by eccentric load. When the balance is in equilibrium the weight of object and comparison standard are the same. The mass may not be the same! Because of air buoyancy 1 kg lead on one side seems to have more weight than 1 kg of feathers on the other side.

This type of balance may have another source of error: The arms may not be of the same length on both sides, caused by inaccurate placing of the joints or temperature effects. This is eliminated in the modern analytical balance:



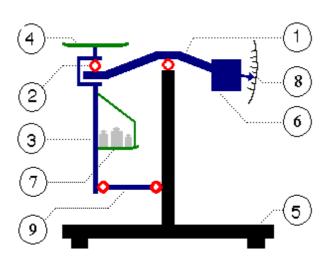
- 1 = arm
- 2 = hinged joint
- 3 = pan carrier
- 4 = weighing pan
- 5 = housing
- 6 = counterweight
- 7 = pan for compensation weights

In this weighing system there is no error caused by difference in armlength: object and compensation weights are on the same arm. The weight of the object is compensated not by placing weights but by removing them. This usually has the form of a rack of weights with a lifting mechanism. The last digits of the weight are mostly read with a pointer which shows the off-balance position of the system.

This type of balance always operates under full load, therefore the hinged joints have to be more

wear resistant (a damaged or worn joint will cause friction and bad reproducibility of results). Air buoyancy still has to be corrected for, like in any other balance that uses comparison-weights with a density different from the object being measured.

A more user-friendly type of balance, especially for pouring in, is the the toploading scale. This works as follows:



1 = arm

2 = hinged joint

3 = pan carrier

4 = weighing pan

5 = housing

6 = counterweight

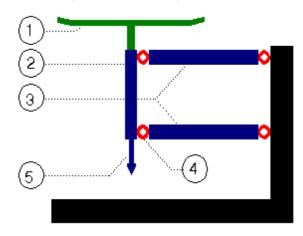
7 = rack with comparison weights

8 = (optional) pointer for last digits

9 = guide

If an object is off-centered on the weighing pan, this causes torque, which generates a counterforce in the suspension guide and arm. If both are parallel the forces in them will not distort the weighing result. Therefore exact adjusting of the joints is important.

In a more plain form this can also be found in modern electronic balances, which use electromagnetic force compensation to obtain their measuring result:



1 = weighing pan

2 = pan carrier

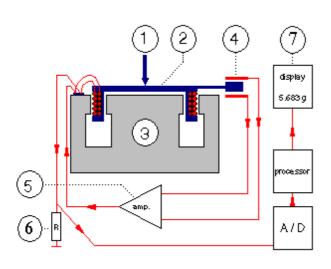
3 = guides

4 = joints

5 =to the force transducer

This works the same in relation to eccentric placing of an object on the pan as in the mechanical toploading scale: the counterforce in the guides will neutralize this, provided they are parallel.

The force transducer works in principle as follows:



1 = direction of the force being measured (and compensated)

2 = coil

3 = permanent magnet

4 = position sensor (null sensor), usually a photocell or capacitive sensor

5 = servo amplifier

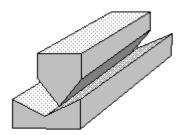
6 = precision resistor (measuring resistor)

7 = digital display

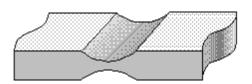
The force on the weighing pan is compensated by the permanent magnet and the magnetic field generated by the current in the coil. This current is regulated by the sensitive position sensor and the servo amplifier, and measured over the precision resistor by the analog-digital converter. For short: the balance measures the current needed to keep the pan

in its position, the pan does not move!

Because the system does not have to move, the joints in an electronic compensating balance, compared to a mechanical balance look quite different:



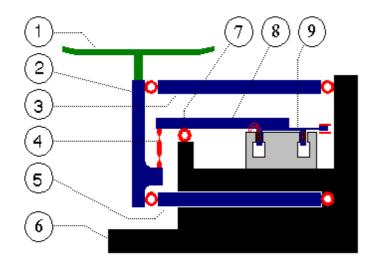
Mechanical balance: a knife on a stone. The touching surface is as thin as possible and very hard to minimize friction. This means that the pressure on this point can be very high, making the balance vulnerable for shocks and vibration.



Electronic compensating balance: The flexible joint is a thinning in the guides (or a leaf spring). Because the system is always brought back to its original position the bending force is of secondary importance, and there is no friction and thus good reproducibility of results. Except when the joint is deformed: the exact position of the "turning point" then becomes dependent of the load and temperature effects.

In the first types of electronic compensating balances the force transducer was placed directly under (or as part of) the pan carrier. This has its limitations: The magnetic fields have to carry the full weight of the system and the object on it and therefore the current in the coil is rather high, causing warming-up of the system and thus temperature effects. Because the magnetic fields of permanent magnet and coil are opposite of each other the field of the magnet might even be completely pushed away by the coil. This can be compensated by adding an extra coil, fixed inside the magnet, working opposite of the first one, but this will bring even more energy into the system, causing more temperature drift.

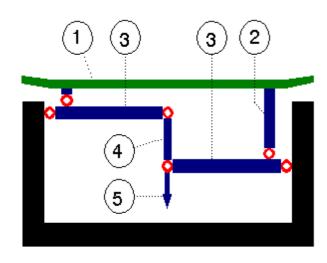
Therefore these older types had a limited weighing range and reading accuracy , and other systems were designed:



- 1 = weighing pan
- 2 = pan carrier
- 3 = upper guide
- 4 = flexible coupling pin
- 5 = lower guide
- 6 = housing
- 7 = flexible joint
- 8 = lever
- 9 = coil

Here the force is transferred to the coil by a lever with a large transmission ratio. The negative effect of the presence of extra joints is much smaller than the positive effect of a lower current in the coil and less possible vertical movement of the guides.

Or for a scale with a large platform: a system with more levers:



1 = weighing platform (pan)

2 = pan carriers

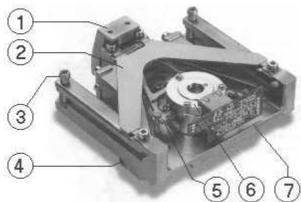
3 = levers

4 = coupling between levers

5 =to the force transducer

If an object is placed on the left-hand side of the platform, a force is applied to the left lever, to the right lever if the object is placed on the right-hand side. If the transmission ratio of both levers is equal, then the force on the transducer is also equal. The same also applies to intermediate positions, in which the forces are transmitted partially by both levers. Thus the readout is independent of the objects position on the weighing pan. A platform scale like this can be over 2m wide and have a weighing range of over 1000kg

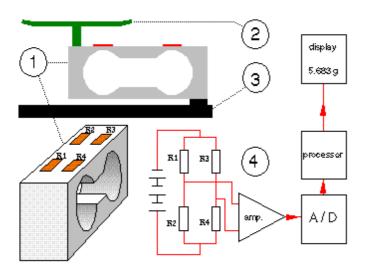
The practical design and construction: Photograph of a weighing system made out of brass for weighing up to 5 kg with 1mg readability.



- 1 = pan carrier (weighing pan removed)
- 2 = upper guide
- 3 = adjustment screws for parallel position of the guides
- 4 = lower guide just visible
- 5 = lever
- 6 = magnet, covered by a magnetic shield with in the center a photocell as position sensor
- 7 = housing block, made out of the same material as guides, lever, and pan carrier to minimize temperature effects.

#### Strain-gauge balances and scales

An method often used for weighing is the strain-gauge balance. These are generally encountered where extremely high resolution is not required (60000 digits or less)(most recent development is 200000 digits for small weights). A strain gauge is a (often zigzag shaped) conductor, etched out of thin metal film. It uses the effect of change in the electrical resistance when it is subjected to mechanical stress, caused by change in length, cross section and specific resistance. Usually, four strain gauges are glued to a "spring body" (flexural component), which is manufactured from a single part, as shown below with its electrical circuit:

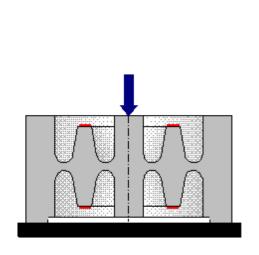


- 1 = spring body (side view and in perspective)
- 2 = weighing pan
- 3 = mounting plate (housing)
- 4 = placing and wiring of the strain gauges (R3 and R4 can also be placed on the under side of the beam)

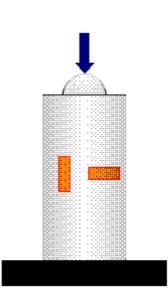
The strain gauges are wired as a Wheatstone-bridge to compensate for temperature changes. When the system is not loaded all four resistors are the same and the input of the amplifier is zero. When an object is placed on the pan R1 and R4 are compressed and their resistance decreases, R2 and R3 are strained and their resistance is increased. This causes a voltage difference at the input of the amplifier, proportional to the weight of the object. The shape if this spring body is comparable with the basic construction of the electronic balance with two guides.

Depending on its maximum load the spring body can also have different shapes, two of which are shown here:

< Cross



section of a double-ring shaped spring body: When a force is applied in the centre the inner ring will tilt, the top being compressed and the under side stretched.



< A cylindrical deforming body: When a force is applied the cylinder will get shorter an the diameter larger. For very heavy loads. Several of these can be placed under a large platform with their output signals being electronically added.

The strain-gauge method of measurement has its limitations for high resolution weighing machines, which are primarily due to creep in the spring material and the adhesive between the spring body and the strain gauges. The moisture sensitivity of the adhesive and the low output signal also cause difficulties. The major advantages of this method are the compact design, cost and its easy adaptability to various maximum capacities.

## Other methods of measurement in weighing technology

**Displacement methods:** Instead of strain-gauge measurement at the bending points, a weighing system with a flexural component can determine the load-dependent displacement of

the load receptor by any given method of displacement measurement. For low accuracy requirements, for instance, inductive transducers are available in which the displacement of coils or ferrite cores is used to generate the weighing signal. For medium accuracy, the change in distance of capacitor electrodes is used. Optical measurement is also possible.

**Magnetic induction:** Under the influence of an external force, some materials alter their magnetic properties; e.g., the permeability drops in the direction of the force. This can be used by bringing two coils, perpendicular to each other, in a block of such material: In unloaded condition, the primary coil induces zero voltage in the secondary coil. Under load, the magnetic-flux lines become asymmetrical and a voltage proportional to the load is induced in the secondary coil. This method is used in scales that weigh in the ton range, particularly under rough conditions.

**Vibrating cord systems:** The resonance frequency of a string is dependent on its length, mass per unit of length, and the tension on it. The tension on the string can also be the weight of an object. As the output signal of such a system is a frequency change, it can be digitized very easily, no analog-digital convertor needed. There is one problem however: The relation between tension force an frequency is not linear. This can be solved digitally by calculating the result, or mechanically by using two vibrating cords. In this case, the quotient of the two cord frequencies is evaluated.

A variation on this is a system that can even be used under weightless conditions: Of a vibrating rod the frequency is also dependent on its length and mass. By placing the sample on a pan at the top of the rod the mass can be evaluated by measuring the change in resonance frequency. Of course the sample has to be attached tightly to the pan!

# Errors, Error calculation and uncertainty.

A deviation in the displayed value from the true value is commonly known as an "error" or "deviation". The standardized term is "error of measurement". In the following, we will use the simpler form "error".

We distinguish between two types of error:

**Systematic errors:** The cause of the error is known, perhaps even the value of this error, or at least an upper limit of error.

Examples:

- A metre rule is not exactly accurate in length; all measurements are made with the same metre rule
- A balance with incorrectly adjusted sensitivity; all measurements carried out on the same balance.
- A measuring instrument is adjusted to 20°C, but the measurement is carried out at 25°C (this is important, e.g., in the case of a volumeter).

**Random errors:** The cause of deviation is either unknown or it is caused by varying influence factors.

Examples:

• Friction in a measuring instrument that has mobile components.

- Fluctuations in the displayed weight, for instance, caused by wind.
- Influence of the operator (parallax errors when reading a display that has a pointer, change in the mass of an object being weighed when the operator touches it with his or her hands).

There is no hard-set difference between systematic and random errors. By means of additional measurements or information, many random errors can be transformed into correctable systematic errors.

#### Example 1: The influence of air pressure on the determination of mass.

The density of air is dependent on air pressure, therefore the buoyancy is dependent on air pressure. If during an extended measuring cycle the momentary air pressure is unknown, this will lead to apparently random fluctuations in results. If the air pressure is measured, the systematic influence can be calculated and corrected accordingly. This means less fluctuation in the weighing results.

# Example 2: Incorrectly adjusted balance: When the same balance is always used this is a systematic error in all measurements.

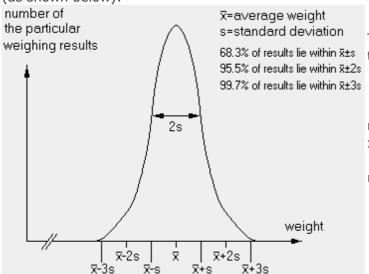
When several balances are available, one of which is incorrectly adjusted, the error will depend on the lab records: without proper statement of the balance being used there is a random error. When the balance used for each measurement was recorded, the error can be calculated and corrected fo accordingly; a known systematic error.

When all balances were adjusted with the same incorrect weight, all measurements will have the same systematic error.

#### **Mathematical rules for random errors**

Rule 1 (statistical distribution): If a measurement is repeated a sufficient number of times and the frequency distribution of the individual values is plotted in a graph, you will obtain a characteristic curve, the so called gaussian curve.

(as shown below):



The standard deviation "s" is given as the quantity for repeatability:

$$S = \sqrt{\frac{1}{n-1} \cdot \sum_{i=1}^{n} \left( X_i - \overline{X} \right)^2}$$

n = total number of measurementsxi = individual results measured= mean value of the individual resultsmeasured:

$$\overline{X} = \frac{1}{n} \cdot \sum_{i=1}^{n} X_i$$

Rule 2 (error propagation for sums and differences): *In sums or differences the squares of the* **absolute** *individual errors are added and the square root of this sum is taken.* 

Example: Container with a tare weight of 205.171g measured with an absolute error of 1mg. After filling, the container measured a gross weight of 210.213g, again with an error of 1mg. This yields a net weight of 210.213g - 205.171g = 5.042g.

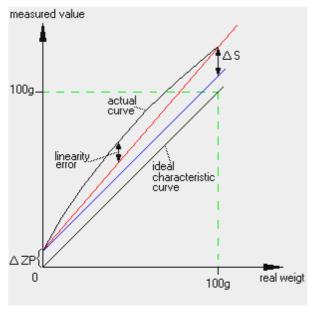
The absolute error of the net weight is: V((1mg)2; + (1mg)2;) = 1.4mg

and the relative error is: 1.4mg / 5.042g = 0.028%Even though the individual measurements reveal only a relative error of 1mg / 200g = 0.0005%, the relative error of the difference increases to 0.028%.

Rule 3 (error propagation for products and quotients): In products or quotients the squares of the **relative** individual errors are added and the square root of this sum is taken. Example: Density determination in accordance with the equation P = mass / volume. measured mass  $P = 150.27 \pm 0.01$ , measured volume V = 173.4cm3;  $\pm 0.1$ cm3; calculated density P = P / V = 150.27 / 173.4 = 0.866609g/cm3;. Error calculation: The relative error of the mass is  $0.01g / 150.27g = 0.666\cdot10^{-4}$ . The relative error of the volume is 0.1cm3; V = 0.1cm4; V = 0.1cm5. The relative error of V = 0.1cm6. V = 0.1cm6. The absolute error of V = 0.1cm6. V = 0.1cm6. V = 0.1cm7. V = 0.1cm9. Thus, the final result is: V = 0.1cm6. V = 0.1cm9. V = 0.1cm9. Thus, the final result is: V = 0.1cm9. V = 0.1cm9.

#### Weighing instrument errors

The actual characteristic curve of a weighing instrument, compared with the ideal characteristic curve, is depicted below (the deviations are greatly exaggerated for better illustration):



The characteristic curve can be shifted by a constant amount, the **zero error**△ZP (the blue line). This error is eliminated by correctly setting the balance to zero before weighing. Therefore, the zero error plays a role only during prolonged measurements, during which the object being weighed cannot be removed from the pan. If the slope of the curve deviates from the ideal characteristic curve (red line), this is known as sensitivity error∆S. A sensitivity error has a negligible effect for small weights or weight differences, but greater for heavier weights. As a result, the sensitivity error is always specified as a relative figure; e.g. 2mg/100g, 20ppm or 20 ·10<sup>-6</sup>/K. A sensitivity error can be caused by temperature drift, aging, adjusting with an incorrect calibration weight, or by incorrect adjustment for compensation of an off-center load error (△S will then be dependent of the position of the sample on the weighing pan). The curve can also be arched: This is known as **linearity error** (or linearity). The maximum linearity is usually listed in the specifications of a balance.

All of these deviations from the ideal can depend on the temperature; this is denoted as the **temperature coefficient** (abbreviated TC). If a data sheet indicates a "sensitivity TC of  $\leq 2.10^{-6}$  /K", this means, for example, that when the sensitivity of the balance is adjusted at 18°C and the balance is subsequently used at 21°C, it can show a sensitivity deviation of (21-18).2·10<sup>-6</sup> = 6·10<sup>-6</sup> maximum, which is the equivalent to 0.6mg/100g.

The effect of aging is known as **long-term drift** of the zero point or sensitivity. If you repeat a weighing procedure under the same ambient conditions, the individual results may deviate slightly from one another. This is known as the **reproducibility** of a weighing

instrument. Expressed as a quantity, this is indicated by the standard deviation "s",

#### Other errors: the effects of moving the balance to a different location.

**Non- horizontal position of the weighing instrument:** Accurate balances are fitted with a spirit level (this is even mandatory on legally verified weighing instruments) for always being able to find back the reference position after moving the instrument: this is the position in which the instrument was correctly adjusted. In the reference position the direction in which the force (the weight) is measured is the same as the direction of gravity. If, for instance, the weighing instrument is moved to a table that is not level, but is tilted 5mm on a length of 1m, and it is not set level again, the direction of measurement deviates 0.2865° from the reference position. The measured weight value W will then be cos0.2865 smaller (W1 = cos0.2865.W = 0.9999875.W), that means on a weight of 200g a 2.5mg lower readout. The zero setting also changes: the zero point is also a weight value, it is the weight of the empty weighing pan.

When in the reference position the direction of measurement exactly coincides with the direction of gravity, the result will always decrease when the instrument is tilted, when this is not the case, the error can be plus or minus. On weighing instruments with a small number of measuring steps (up to about 10000 digits) the influence of a not horizontal position under normal circumstances is negligible, therefore these often don't have a spirit level: "level on the face of it" will then be good enough. On a classical two-armed balance the effect is again different: on the comparison of two weights there will be no influence, both scales will always hang straight below the measuring point (suspension point). But if the last digits of the difference between the weights are read by a pointer on the arm an error will occur in the sensitivity of this pointing device.

**Moving the weighing instrument in height:** As the force of attraction (= gravity) between two objects (the earth and the object being weighed) depends on their distance, the measured value will change when the weighing instrument is moved to a different height. By every meter elevation (at moderate heights) the field of gravity changes from sea level -0.3086·10<sup>-6</sup> N/(mkg). Or as a more practical figure: when the weighing instrument is placed one floor higher (about 4m), a weight of 200g will weigh 0.26mg less.

**Moving over a larger distance:** The acceleration of gravity **g** is not the same everywhere on earth: As a consequence of centrifugal forces caused by the earth's rotation it is less at the equator than at the poles. Also the earth is not a perfect sphere: the distance from the surface to the earth's center of gravity is larger at the equator than at the poles.

The absolute deviation caused by moving the instrument can be considerable larger than the error of the weights used for adjustment (and larger than the maximum permissible errors for verified weighing instruments). Therefore after moving to a different location readjustment is necessary. Many weighing instruments are fitted with a built-in adjustment weight for this purpose: with this the sensitivity deviation caused by relocating the instrument is easily corrected.

#### Other errors: forces working on an object being weighed.

**Air currents / drafts:** These are often the cause of large random errors, as the effect of air currents depends on unpredictable circumstances like the shape and size of the object being weighed, posture and movements of the operator, or opening doors. Sometimes the metrological

demand for the least possible air currents collides with safety requirements: Poisonous substances must be weighed in a fume cupboard. To minimize the effect of ambient air flow, draft shields are used. For balances with a readability of 1mg, an open draft shield, e.g., in the shape of a glass cylinder, will suffice under normal conditions. Balances with a readability of 0.1mg or less require a closed draft shield. Contrary to practical considerations, a draft shield should be as small as possible from a metrological viewpoint, because internal drafts can be generated within a large draft shield chamber.

A special case of air-current effect is what happens when the object being weighed does not have the same temperature as the balance an the surrounding air: Convection currents will make objects that are hotter appear to be lighter and those that are colder, heavier. Only when the shape, surface, and temperature of the object is exactly known, this will be a quantifiable error (see under the chapter "tables" the one about the temperature effects on weights). It is always important to condition an object being weighed to the ambient temperature!

**Adsorptive layer of moisture on the surface:** Allowing an object sufficient time to reach the same temperature as that of the weighing instrument is also necessary in order for the adsorptive layer of moisture on the surface of the object to equilibrate. Particularly when small objects are weighed on a high-resolution balance, this is essential to obtain reproducible weighing results. To minimize adsorption of humidity, users must avoid soiling or otherwise touching the objects with their hands, for example, as this leaves fingerprints, which can affect the weighing results (a fingerprint does not only have a weight of its own of 0.1 - 1mg, but is also very hygroscopic).

**Electrostatic forces:** These are generated when nonconductive objects or containers (glass or plastic) are electrically charged, for example, by pouring from one container to another or by air currents. Static electricity can be prevented by maintaining sufficient air humidity (at least 60%), or by using an electrically conductive enclosure that is connected to the weighing pan. Other solutions: Let the sample condition on a metal plate that is connected to the same electrical ground as the balance, ionize the air in and around the balance with an ionizing blower, don't use a plastic draft shield or sample container: plastics are more easily electrically charged than glass.

Electrostatic forces usually show up as a drift in the weighing results (the balances readout seems to stand still after placing the sample on the pan, but than slowly starts to drift in <u>one</u> direction), or in poor reproducibility in repeated weighing procedures.

**Magnetic forces** that act on an object being weighed can be counteracted only by carefully demagnetizing the object, by shielding the magnetically active object using soft magnetic materials such as mumetal, or by keeping the object at sufficient distance from all magnetic or magnetizable parts. Weighing instruments with electromagnetic force compensation contain magnetic parts (which are usually well shielded), but even on a mechanical balance the earths magnetic field can have a considerable effect on a magnetized sample. Magnetic forces generally manifest themselves in poor reproducibility of the results and, particularly, in a strong dependency of the position of the object on the weighing pan. An often made mistake is weighing a liquid sample with a magnetic stirrer still in it: This can only be done on a specially prepared scale that always keeps bottle and stirrer in the same position and compensates for the error, or a scale that weighs while stirring; the error than becomes an alternating effect which can be filtered out.

**Air buoyancy:** An effect which is often underestimated, is air buoyancy: Every object is subject to an upward force, which is equal to the weight of the displaced air. Therefore, this force will be larger on an object with a large volume (low density), and smaller on an object with high

density. A weighing instrument compares two forces; the force exerted on the pan by the object being weighed, and the force exerted by the standard weight that was used to adjust the instrument (or the compensation weights in the case of a mechanical balance). The effect is a difference in display dependent on the density of the object, as depicted in the following graph:

As shown by the green dotted line: When 10g of water (density 1.0) is weighed at an average air density, the real mass of the water in the container is 10.5mg higher than the displayed value; a considerable difference. When air pressure and temperature change, the air density will also change. In the example above this can increase the difference up to 11.5mg or  $\rho$ =5.0 g/cm<sup>3</sup> decrease down to 9.5mg. If the sample has a density of  $\rho$ = 8.0 g/cm<sup>3</sup> 8.0g/cm3;, which is the same as  $\rho$ = 15 g/cm<sup>3</sup> the weight used for adjustment, the displayed mass will be the same as the real mass (the flat line in the graph).

# The effect of air buoyancy can be calculated by the following equations:

The force of air buoyancy "A" is equal to the weight (force) of the displaced air:

$$A = m_A \cdot g = V_m \cdot \rho_A \cdot g = \frac{m}{\rho_w} \cdot \rho_A \cdot g = m \cdot \frac{\rho_A}{\rho_w} \cdot g = m \cdot \frac{\rho_A}{\rho$$

The readout of the weighing instrument "mw" can be calculated from the real mass "m" in this way:

$$m_{w} = m \cdot \frac{1 - \frac{\rho_{A}}{\rho_{w}}}{1 - \frac{\rho_{A}}{\rho_{s}}} \xrightarrow[\rho_{A}]{m_{w} = displayed \ value} \\ m = real \ mass \ of \ the \\ object \\ \rho_{A} = air \ density$$
 max = density of the object 
$$\rho_{S} = density \ of \ the \ object \\ \rho_{S} = density \ of \ the \ object \\ object \\ instrument$$
 (this is standardized to 8.000 g/cm&3;).

Resolved to the real mass "m" the equation above yields:

$$m = m_w \cdot \frac{1 - \frac{\rho_A}{\rho_s}}{1 - \frac{\rho_A}{\rho_{o...}}}$$

There are several ways to determine the air density "%", both by calculation and measurement:

In accordance with the equation recommended by the "Comité International des Poids et Mesures", for the air density &, the equation between numerical values yields the following:

$$\rho_{A} = 0.3485 \cdot \frac{p}{T} - 1.32 \cdot 10^{-3} \cdot p_{s} \cdot \frac{\varphi}{T}$$

Where:

R = air density in kg/m&3;

p = barometric pressure in Pa

T = air temperature in Kelvin

Z = real gas factor (Z = 0.9996....0.9997 between 15°C and 25°C and p = 0.1MPa

Xco2 = content of CO2 in % by volume

Xv =molar fraction of water vapor

As the molar fraction of the water vapor is generally unknown, and only the relative humidity is known, the following formula for approximation is frequently used:

$$\rho_{A} = 0.3485 \cdot \frac{p}{T} - 1.32 \cdot 10^{-3} \cdot p_{s} \cdot \frac{\phi}{T}$$

Where:

R = air density in kg/m3;

p = barometric pressure in mbar

T = temperature in Kelvin (T = 273.15 + t, t = temperature in °C)

Q= relative humidity in %

Ps = saturation vapor pressure of water in mbar, according to the following table:

Temperature t in °C	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Ps in mbar	12.28	13.13	14.03	14.98	15.99	17.05	18.18	19.38	20.64	21.98	23.39	24.87	26.44	28.10	29.85	31.69	33.63	35.67	37.82	40.08	42.45

This will yield a value for the air density with an accuracy of 3 decimals, depending on the accuracy of the measurements used. More accurate calculations are possible; for this refer to various textbooks.

Another possibility is measuring the air density directly using a balance and two objects of (about the same) known mass m1 and m2 and different known volumes V1 and V2. The difference of measured weight of these two objects will be:

$$\Delta = m_1 - m_2 + \rho_A \cdot (\nabla_2 - \nabla_1)$$

If the test objects have exactly the same mass and a difference in volume V1-V2 = 1 cm<sub>3</sub>; exactly, the displayed difference  $\Delta$  is equal to the air density in g/cm<sub>3</sub>;.

Sartorius supplies a set of two test weights with different densities for air density determination. In addition, the Sartorius MC-series of microbalances features a built-in software program called "Eureka" for air buoyancy correction. This program allows both air density determination and buoyancy correction without the need for pocket calculators or external computers.

# **Tables and Figures**

# Common legal units, multiples and parts of the kilogram:

Unit	Unit symbol	Relation to the base unit
Nanogram	ng	$1 \text{ ng} = 1.10^{-12} \text{ kg}$
Microgram	μg	$1 \mu g = 1.10^{-9} \text{ kg}$
Milligram	mg	1 mg = 1·10 <sup>-6</sup> kg
Gram	g	1  g = 1/1000  kg
Kilogram	kg	base unit
Ton	t	1 t = 1000 kg
Carat	ct	$1 \text{ ct} = 20 \text{ mg} = 20 \cdot 10^{-6} \text{ kg}$

Remark: The carat is only allowed as a unit for weighing gold, pearls and precious stone.

# Anglo-American and other weight units:

Unit	Symbol	1 kg =	1 (unit) =
Pound	lb	2.2046 LB	453.595 g

Ounce	oz	35.274 oz	28.349 g	
Troy ounce	oztr	32.1505 oztr	31.104 g	
Grain	gn (gr)	15432 gn	0.06480 g	
Pennyweights	dwt	643.02 dwt	1.55517 g	
Mesghal	m	217.00 m	4.6083 g	
Momne	m	266.70 m	3.7495 g	
Tola	t	85.733 t	11.664 g	
Baht	b	65.790 b	15.200 g	
Hongkong Teals	TL	26.717 TL	37.429 g	
Singapore Teals	TL	26.461 TL	37.792 g	
Taiwanese Teals	TL	26.667 TL	37.500 g	
Chinese Teals	TL	26.455 TL	37.799 g	
Carat ( Karat )	CT (k)	50000.0 CT	0.02000 g	

# VISIT OUR COMPREHENSIVE UNIT CONVERSION CENTRE A brief history of balances Refer to the section on terms and definitions

# **Error limits for calibration weights (OIML R111)**:

# Maximum error limits in mg (deviation + uncertainty) for accuracy classes E1, E2, F1, F2, M1

1 2, 111						
Nominal mass value	Class E1	Class E2	Class F1	Class F2	Class M1	
50 kg	25	75	250	750	2500	
20 kg	10	30	100	300	1000	
10 kg	5	15	50	150	500	
5 kg	2.5	7.5	25	75	250	
2 kg	1.0	3.0	10	30	100	
1 kg	0.5	1.5	5	15	50	
500 g	0.25	0.75	2.5	7.5	25	
200 g	0.10	0.30	1.0	3.0	10	
100 g	0.05	0.15	0.5	1.5	5	
50 g	0.030	0.10	0.30	1.0	3.0	
20 g	0.025	0.080	0.25	0.8	2.5	
10 g	0.020	0.060	0.20	0.6	2.0	
5 g	0.015	0.050	0.15	0.5	1.5	
2 g	0.012	0.040	0.12	0.4	1.2	
1 g	0.010	0.030	0.10	0.3	1.0	

500 mg	0.008	0.025	0.08	0.25	0.8
200 mg	0.006	0.020	0.06	0.20	0.6
100 mg	0.005	0.015	0.05	0.15	0.5
50 mg	0.004	0.012	0.04	0.12	0.4
20 mg	0.003	0.010	0.03	0.10	0.3
10 mg	0.002	0.008	0.025	0.08	0.25
5 mg	0.002	0.006	0.020	0.06	0.20
2 mg	0.002	0.006	0.020	0.06	0.20
1 mg	0.002	0.006	0.020	0.06	0.20

Influence of non temperature- acclimatized weights:

Weight value >	50 g	100 g	200 g	500 g	1 kg
Maximum deviation of the weight for class E1	0.030 mg	0.05 mg	0.10 mg	0.25 mg	0.50 mg
Maximum deviation of the weight for class E2	0.10 mg	0.15 mg	0.30 mg	0.75 mg	1.5 mg
Maximum deviation of the weight for class F1	0.30 mg	0.5 mg	1.0 mg	2.5 mg	5 mg
Displayed error at 10 K temperature difference	0.3 mg	0.6 mg	0.8 mg	1.6 mg	2.5 mg
Displayed error at 5 K temperature difference	0.15 mg	0.3 mg	0.4 mg	0.8 mg	1.2 mg
Half-life time of the error	9 min.	12 min.	20 min.	35 min.	60 min.

As shown by these figures, the influence of temperature difference between the weight and the ambient air can be considerably larger than the uncertainty of the weight itself. Therefore weights must be acclimatized before use. When class E1 or E2 weights are used, they must be placed next to the weighing instrument for several hours to acclimatize, otherwise it does not make sense to calibrate with this high accuracy: The error caused by even small temperature differences can be larger than the error of the weight.

## Accuracy classes of weighing equipment

			number of verification scale intervals <b>e</b>	number of verification scale intervals <b>e</b>
class	verification scale interval <b>e</b>	minimum capacity	minimum n = min. / e	maximum n = max / e
I	0.001g ≤ <b>e</b>	100 <b>e</b>	50 000	no maximum
II	$0.001g \le \mathbf{e} \le 0.05g$ $0.1g \le \mathbf{e}$	20 <b>e</b> 50 <b>e</b>	100 5 000	100 000 100 000
III	0.1g ≤ <b>e</b> ≤ 2g 5g ≤ <b>e</b>	20 <b>e</b> 20 <b>e</b>	100 500	10 000 10 000

# For scales with different scale intervals:

i = 1, 2, etc. = number of the partial weighing range

			number of verification scale intervals <b>e</b>	number of verification scale intervals <b>e</b>
class	verification scale interval <b>e</b>	minimum capacity	minimum n = maxi / <b>e</b> i	maximum n = maxi / <b>e</b>
I	0.001g <b>≤ e</b> i	100 <b>e</b> 1	50 000	no maximum
II	0.001g ≤ <b>e</b> i≤ 0.05g 0.1g ≤ <b>e</b> i	20 <b>e</b> 1 50 <b>e</b> 1	5 000 5 000	100 000 100 000
III	0.1g <b>≤ e</b> i	20 <b>e</b> 1	500	10 000

## maximum permissible errors:

Class I	Class II	Class III	Maximum permissible error:
0 ≤ m ≤ 50 000 <b>e</b>	0 ≤ m ≤ 5 000 <b>e</b>	0 ≤ m ≤ 500 <b>e</b>	± 0.5 <b>e</b>
50 000 <b>e</b> < m ≤ 200 000 <b>e</b>	5 000 <b>e</b> < m ≤ 20 000 <b>e</b>	500 <b>e</b> < m ≤ 2 000 <b>e</b>	± 1.0 <b>e</b>
200 000 <b>e</b> < m	20 000 <b>e</b> < m ≤ 10 000 <b>e</b>	2 000 <b>e</b> < m ≤ 10 000 <b>e</b>	± 1.5 <b>e</b>

These are maximum permissible errors on initial verification. The maximum permissible errors "in use" are twice these errors.

# Variations in gravity (g) within Holland

Town	g in N/kg
Groningen	9,81331
Den Helder	9,81324
Zwolle	9,81290
Amsterdam	9,81273
Utrecht	9,81251
Delft	9,81241
Dordrecht	9,81226
's Hertogenbosch	9,81199
Middelburg	9,81205
Maastricht	9,81127

Local differences caused by variations in the density of the underground can be up to 1·10<sup>-4</sup> relative. Data taken from report of Technical University Delft.

Information supplied by courtesy of Zeegert van Huissteden. an engineer with Sartorius Netherlands